

Weak form of bond-associated peridynamics for finite elastic deformation and rupture in rubber-like materials

D. Behera, P. Roy and E. Madenci
University of Arizona, Tucson, AZ

Workshop on Experimental and Computational Fracture Mechanics
Baton Rouge, Louisiana, February 26-28, 2020

Outline

- **Existing models**
- **Peridynamic (PD) theory**
- **Bond-associated deformation gradient**
- **Weak form of PD**
- **Numerical results**
- **Remarks**

Existing models

FEA with criteria for crack initiation and propagation

- J-integral criteria (Hocine et al., 1998, 2002, 2003),
- Local energy release rate criteria (Mzabi et al., 2011)
- Strain energy density (SED) criteria (Hamdi et al., 2007)
- Local (or average) SED criteria (Berto, 2015)
- Tearing energy (Rivlin and Thomas, 1953 and Pidaparti et al., 1990)
- Maximum principal stretch and stress (Hamdi et al., 2007)
- Effective stretch (Ayatollahi et al., 2016)

Such criteria are based on local stress and strain fields

Predictions are significantly influenced by the mesh size

FEA coupled with a phase-field approach (Talamini et al., 2018)

- Length scale to predict the rupture process
- Phase-field is driven only by the internal energy of polymer

It successfully describes damage initiation, propagation, and rupture

Existing peridynamic models

PD form of strain energy density functions

- Tearing of a rubber sheet (Silling and Bobaru (2005))
- Uniform stretch of a rubber sheet w/o failure (Bang and Madenci, 2017)
- 3D simulation of hyperelastic materials w/o failure (Xu et al., 2018)
- Visco-hyperelastic deformation of polymers (Huang et al., 2019)

Classical form of strain energy density functions

- Arruda-Boyce model w/o failure (Henke, 2013)
- Neo-Hookean model w/o failure (Waxman and Guven, 2020)

Peridynamic theory

As horizon approaches zero, it recovers local theory

$$\nabla \cdot \boldsymbol{\sigma} + \mathbf{b}(\mathbf{x}, t) = \rho \ddot{\mathbf{u}}(\mathbf{x}, t)$$

Failure initiation and growth through removal of interactions

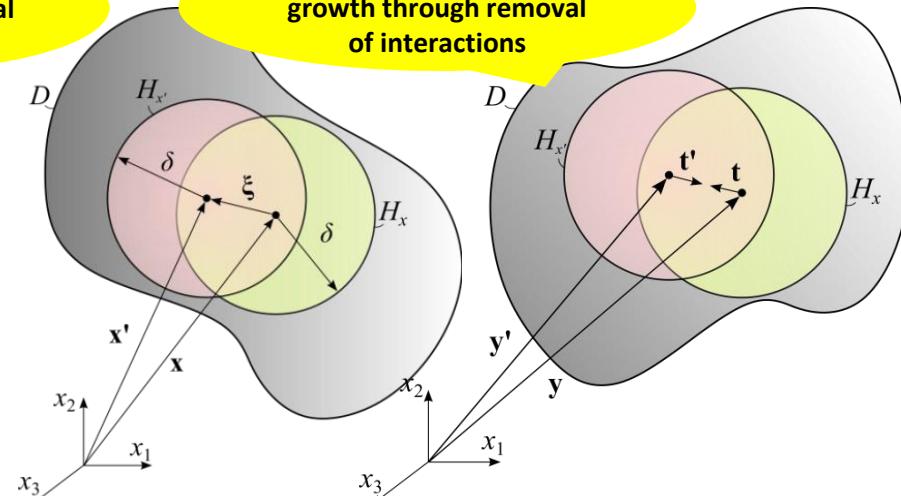
$$\int_{H_x} (\mathbf{t} - \mathbf{t}') dV + \mathbf{b}(\mathbf{x}, t) = \rho \ddot{\mathbf{u}}(\mathbf{x}, t)$$

$$\mathbf{t}(\mathbf{x}) = w(|\xi|) \mathbf{P} \mathbf{K}^{-1} \xi$$

$$\mathbf{K} = \int_{H_x} w(|\xi|) (\xi \otimes \xi) dV_{x'}$$

No spatial derivatives
Internal length parameter
Valid at discontinuities

$$\mathbf{P}(\mathbf{F}) = \frac{\partial \Psi(\mathbf{F})}{\partial \mathbf{F}}$$



Boundary conditions
Displacement constraints - natural
Nonzero tractions - body forces
Zero tractions - Lagrange mult.

PD form of deformation gradient

Silling et al. (2007) - “*reduction*” process

$$\mathbf{y}' = \mathbf{y} + (\nabla \mathbf{y}(\mathbf{x})) \xi + R(1, \mathbf{x})$$

$$\mathbf{y}' - \mathbf{y} = \mathbf{F}(\mathbf{x}) \xi$$

$$(\mathbf{y}' - \mathbf{y}) \otimes \xi = \mathbf{F}(\mathbf{x}) (\xi \otimes \xi)$$

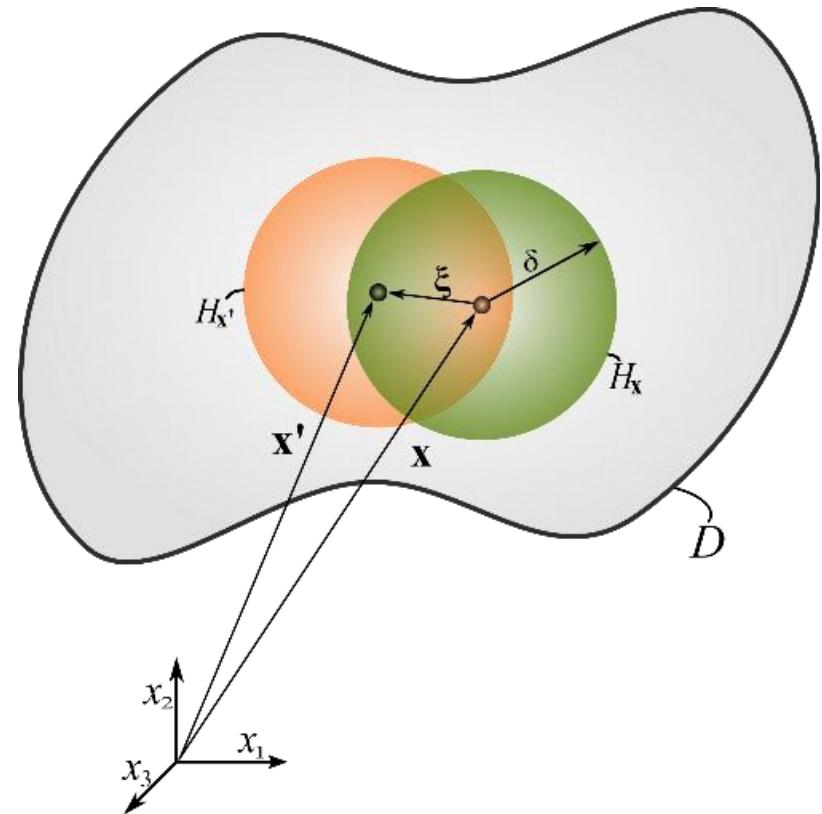
$$\int_{H_x} w(|\xi|) (\mathbf{y}' - \mathbf{y}) \otimes \xi dV_{x'} = \mathbf{F}(\mathbf{x}) \mathbf{K}(\mathbf{x})$$

$$\mathbf{K}(\mathbf{x}) = \int_{H_x} w(|\xi|) (\xi \otimes \xi) dV_{x'}$$

$$\mathbf{F}(\mathbf{x}) = \left(\int_{H_x} w(|\xi|) (\mathbf{y}' - \mathbf{y}) \otimes \xi dV_{x'} \right) \mathbf{K}^{-1}$$

$$\mathbf{F}(\mathbf{x}) = \int_{H_x} (\mathbf{y}' - \mathbf{y}) \otimes \mathbf{g} dV_{x'}$$

$$\mathbf{g} = w(|\xi|) \mathbf{K}^{-1} \xi$$



Silling et al. , 2007, “Peridynamics states and constitutive modeling,” J. Elasticity, 88 : 151-184

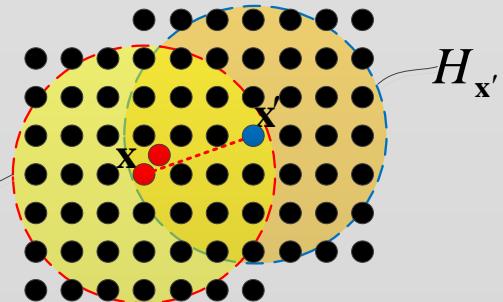
$\mathbf{F}(\mathbf{x})$ at two different states

$$\mathbf{y}_{\text{new}}(\mathbf{x}) = \mathbf{y}_{\text{old}}(\mathbf{x}) + \mathbf{u}_d(\mathbf{x})$$

$$\mathbf{y}_{\text{new}}(\mathbf{x}') = \mathbf{y}_{\text{old}}(\mathbf{x}')$$

$$\mathbf{F}_{\text{old}}(\mathbf{x}) = \left(\int_{H_x} w(|\xi|) (\mathbf{y}_{\text{old}}(\mathbf{x}') - \mathbf{y}_{\text{old}}(\mathbf{x})) \otimes (\mathbf{x}' - \mathbf{x}) dV_{\mathbf{x}'} \right) \mathbf{K}^{-1}(\mathbf{x})$$

R



$$\mathbf{F}_{\text{new}}(\mathbf{x}) = \left(\int_{H_x} w(|\xi|) (\mathbf{y}_{\text{new}}(\mathbf{x}') - \mathbf{y}_{\text{new}}(\mathbf{x})) \otimes (\mathbf{x}' - \mathbf{x}) dV_{\mathbf{x}'} \right) \mathbf{K}^{-1}(\mathbf{x})$$

$$\mathbf{F}_{\text{new}}(\mathbf{x}) = \left(\int_{H_x} w(|\xi|) (\mathbf{y}_{\text{new}}(\mathbf{x}') - (\mathbf{y}_{\text{old}}(\mathbf{x}) + \mathbf{u}_d(\mathbf{x}))) \otimes (\mathbf{x}' - \mathbf{x}) dV_{\mathbf{x}'} \right) \mathbf{K}^{-1}(\mathbf{x})$$

Uniform discretization and a spherically symmetric influence function

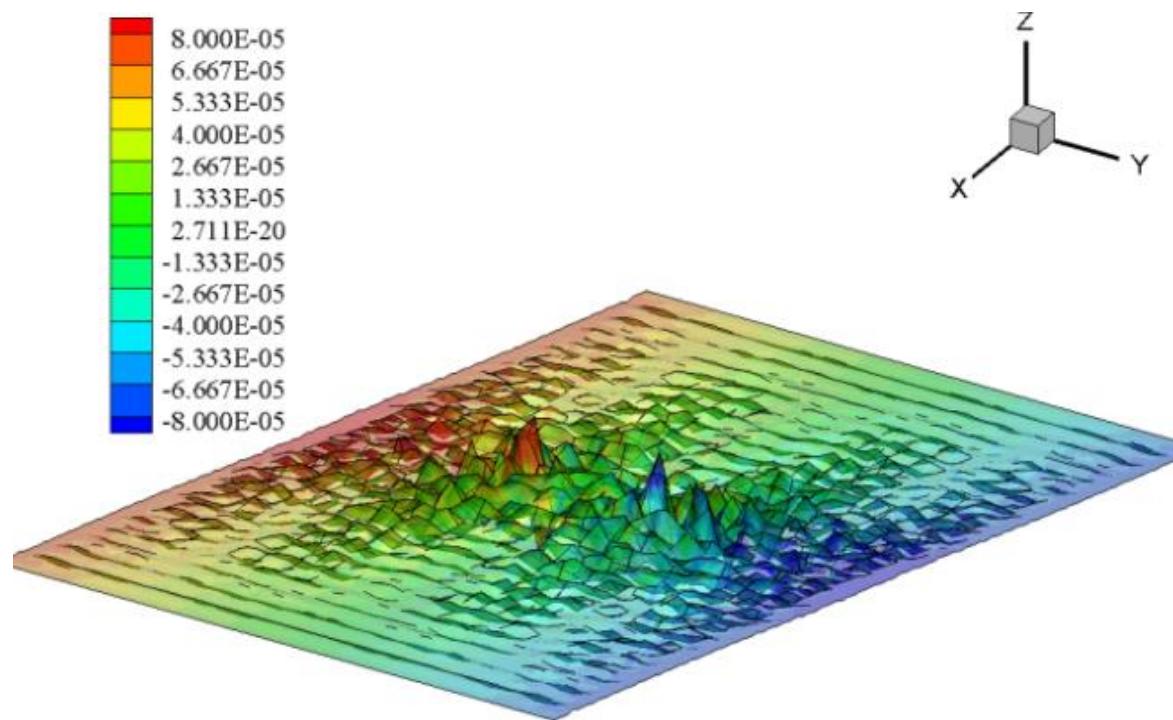
$$\mathbf{F}_{\text{new}}(\mathbf{x}) = \mathbf{F}_{\text{old}}(\mathbf{x}) - \mathbf{u}_d(\mathbf{x}) \otimes \underbrace{\left(\int_{H_x} w(|\xi|) (\mathbf{x}' - \mathbf{x}) dV_{\mathbf{x}'} \right)}_{=0} \mathbf{K}^{-1}(\mathbf{x})$$

Zero deformation energy due to a displacement variation

Zero-energy deformation mode

Zero-energy deformation modes

- Numerical instability/oscillation - in regions of steep deformation gradient such as a crack
- Stabilization techniques - artificial

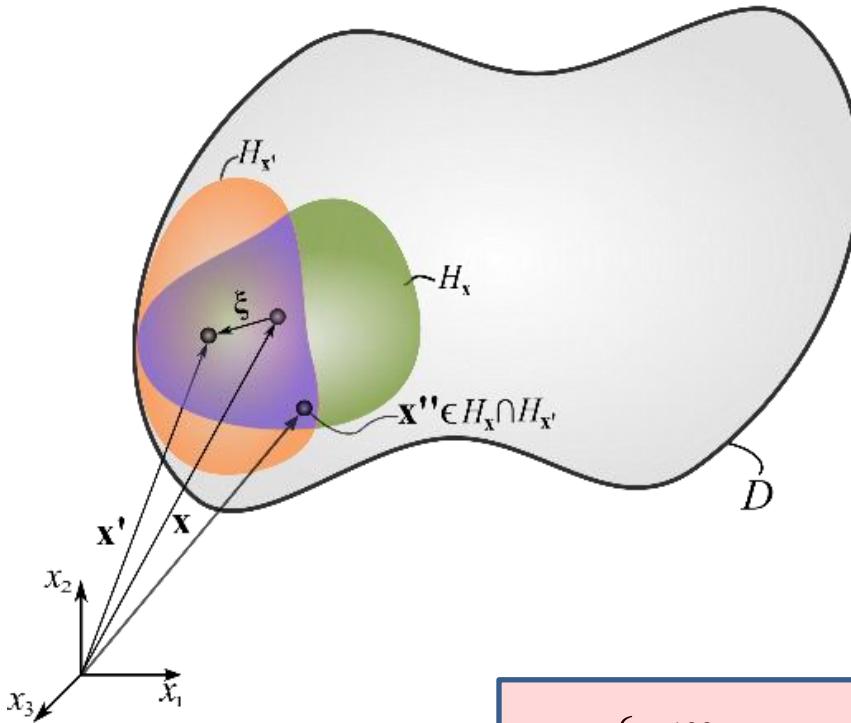


Numerical stabilization techniques

- Enhanced integration methods
- Adding an extra force vector state (damping term)
- Suitable influence function
- Averaging/Smoothing displacement field
- Higher-order approximation deformation gradient
- Stress point method
- Sub-horizon average method
- Variable correction method at bond-level
- Bond-associated horizon
- Bond-associated deformation gradient
 - Disturbs the radial symmetry and removes the zero-energy mode

Chen H, Bond-associated deformation gradients for peridynamic correspondence model. Mechanics Research Comm., 2018, 90:34-41.
Chen H and Spencer BW, Peridynamic Bond-Associated Correspondence Model: Stability and Convergence Properties. IJNME, 2018; 117, 713-723

Bond-associated deformation gradient



$$\mathbf{F}_\xi(\mathbf{x}) = \int_{H_x \cap H_{x'}} (\mathbf{y}'' - \mathbf{y}) \otimes \mathbf{g}_\xi dV_{x''}$$

$$\mathbf{g}_\xi = \begin{Bmatrix} g_1^{100}(\xi; w(|\xi|)) \\ g_1^{010}(\xi; w(|\xi|)) \\ g_1^{001}(\xi; w(|\xi|)) \end{Bmatrix}$$

Chen H, Bond-associated deformation gradients for peridynamic correspondence model. Mechanics Research Comm., 2018, 90:34-41.

Chen H and Spencer BW, Peridynamic Bond-Associated Correspondence Model: Stability and Convergence Properties. IJNME, 2018; 117, 713-7273

Madenci E, Barut A, Dorduncu M, Peridynamic Differential Operator for Numerical Analysis, Springer, 2019.

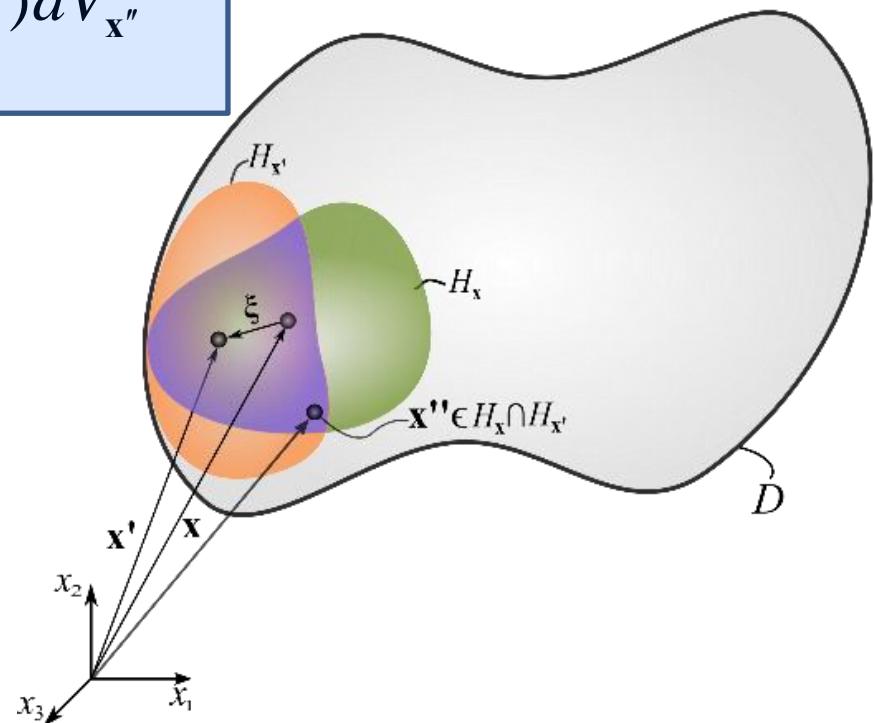
Bond strain energy density

$$\delta W_{\xi}^{PD}(\mathbf{x}) = \frac{1}{2} \int_{H_{\mathbf{x}} \cap H_{\mathbf{x}''}} (\mathbf{t}_{\xi}(\mathbf{x}) - \mathbf{t}_{\xi}(\mathbf{x}'')) \cdot \delta(\mathbf{y}(\mathbf{x}'') - \mathbf{y}(\mathbf{x})) dV_{\mathbf{x}''}$$

$$\delta W_{\xi}^{CCM}(\mathbf{x}) = \int_{H_{\mathbf{x}} \cap H_{\mathbf{x}''}} (\mathbf{P}_{\xi} \mathbf{g}_{\xi})^T \delta(\mathbf{y}'' - \mathbf{y}) dV_{\mathbf{x}''}$$

$$\delta W_{\xi}^{CCM}(\mathbf{x}) = \text{tr}(\mathbf{P}_{\xi}^T \delta \mathbf{F}_{\xi})$$

$$\mathbf{P}_{\xi} = \frac{\partial \Psi(\mathbf{F}_{\xi})}{\partial \mathbf{F}_{\xi}}$$



Equating PD and classical SED

$$\delta W_{\xi}^{PD}(\mathbf{x}) = \phi_{\xi}(\mathbf{x}, \mathbf{x}') \delta W_{\xi}^{CCM}(\mathbf{x})$$

Assumption

$$\phi_{\xi}(\mathbf{x}, \mathbf{x}') = \frac{\int_{H_{\mathbf{x}} \cap H_{\mathbf{x}'}} dV_{\mathbf{x}''}}{\int_{H_{\mathbf{x}}} dV_{\mathbf{x}''}}$$

$$\mathbf{L}^{PD}(\mathbf{x}, t) = \int_{H_{\mathbf{x}}} \left(\phi_{\xi}(\mathbf{x}, \mathbf{x}') \mathbf{P}_{\xi} \mathbf{g}_{\xi}(\mathbf{x}) - \phi_{\xi}(\mathbf{x}', \mathbf{x}) \mathbf{P}'_{\xi} \mathbf{g}_{\xi}(\mathbf{x}') \right) dV_{\mathbf{x}'}$$

Chen H, Bond-associated deformation gradients for peridynamic correspondence model. Mechanics Research Comm., 2018, 90:34-41.

Chen H and Spencer BW, Peridynamic Bond-Associated Correspondence Model: Stability and Convergence Properties. IJNME, 2018; 117, 713-7273

Neo-Hookean material model

$$\Psi(\bar{I}_1, J) = \frac{\mu}{2} (\bar{I}_1 - 3) + \frac{K}{8} \left(J - \frac{1}{J} \right)^2$$

$$\bar{I}_1 = \frac{\text{tr}\mathbf{C}}{J^{2/3}} \quad \mathbf{C} = \mathbf{F}^T \mathbf{F} \quad J = \det \mathbf{F}$$

$$\mathbf{P} = \frac{\partial \Psi}{\partial \mathbf{F}} = \mu \left(\mathbf{F} - \frac{1}{3} \text{tr}\mathbf{C}\mathbf{F}^{-T} \right) J^{-2/3} + \frac{K}{4} (J^2 - J^{-2}) \mathbf{F}^{-T}$$

$$\mathbf{P} = \mu \left(\mathbf{F} - \frac{1}{2} \text{tr}\mathbf{C}\mathbf{F}^{-T} \right) J^{-1} + \frac{K}{4} (J^2 - J^{-2}) \mathbf{F}^{-T} \quad \text{-- plane strain}$$

$$\mathbf{P} = \mu \left(\mathbf{F} - \frac{1}{3} C_{33} \mathbf{F}^{-T} \right) J^{-2/3} \quad \text{-- plane stress}$$

Weak form of Peridynamics

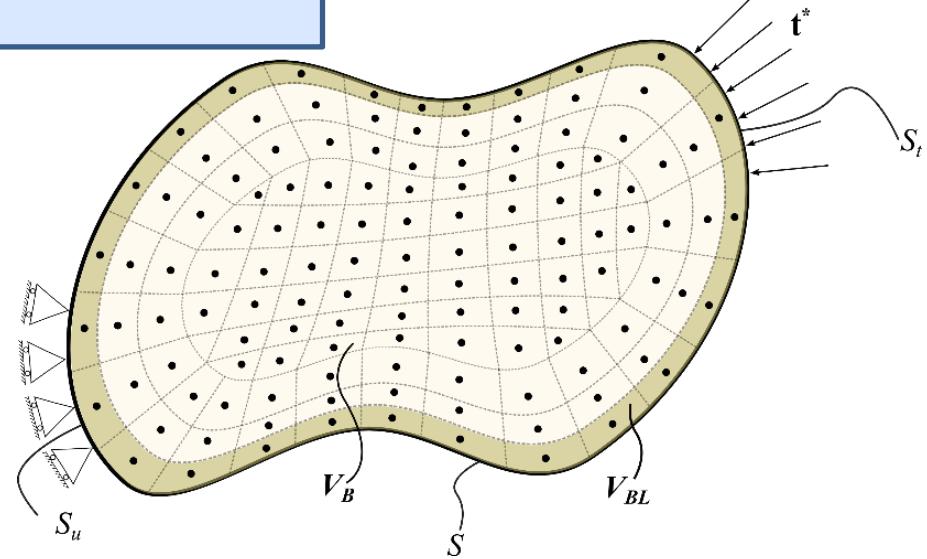
$$\delta U + \delta V = 0$$

$$\oint_{\Gamma} (\mathbf{P}^{\text{PD}} \mathbf{n}) \cdot \delta \mathbf{u} dS - \int_A \mathbf{L}^{\text{PD}} \cdot \delta \mathbf{u} dV - \int_{\Gamma_t} \mathbf{t}^* \cdot \delta \mathbf{u} dS = 0$$

$$\int_A \mathbf{L}^{\text{PD}} \cdot \delta \mathbf{u} dA \approx \delta \mathbf{V}^T \mathbf{Q}$$

$$\int_{\Gamma} (\mathbf{P}^{\text{PD}} \mathbf{n}) \cdot \delta \mathbf{u} d\Gamma = \delta \mathbf{V}_{\text{BL}}^T \mathbf{q}_{\text{BL}}$$

$$\int_{\Gamma_t} \mathbf{t}^* \cdot \delta \mathbf{u} d\Gamma = \delta \mathbf{V}_t^T \mathbf{q}_t^*$$



$$\mathbf{V} = \begin{Bmatrix} \mathbf{V}_B & \mathbf{V}_{BL} \end{Bmatrix}^T = \begin{Bmatrix} \mathbf{V}_B & \mathbf{V}_t & \mathbf{V}_u \end{Bmatrix}^T$$

$$\mathbf{Q} = \begin{Bmatrix} \mathbf{Q}_B & \mathbf{Q}_{BL} \end{Bmatrix}^T = \begin{Bmatrix} \mathbf{Q}_B & \mathbf{Q}_t & \mathbf{Q}_u \end{Bmatrix}^T$$

$$\mathbf{q}_{BL} = \begin{Bmatrix} \mathbf{q}_t & \mathbf{q}_u \end{Bmatrix}^T$$

$$\left\{ \mathbf{Q}_B \quad (\mathbf{Q}_t - \mathbf{q}_t + \mathbf{q}_t^*) \quad (\mathbf{Q}_u - \mathbf{q}_u) \right\} \begin{Bmatrix} \delta \mathbf{V}_B \\ \delta \mathbf{V}_t \\ \delta \mathbf{V}_u \end{Bmatrix} = 0$$

Madenci, E., Dorduncu, M., Barut, A. and Phan, N., 2018, "Weak form of peridynamics for nonlocal essential and natural boundary conditions," CMAME, Vol. 337, pp. 598-631.

Nonlinear governing equations

$$\mathbf{R}(\mathbf{V}; \mathbf{f}_t^*) = \begin{Bmatrix} \mathbf{Q}_B \\ \mathbf{Q}_t - \mathbf{q}_t + \mathbf{q}_t^* \\ \mathbf{Q}_u - \mathbf{q}_u \end{Bmatrix} = \begin{Bmatrix} \mathbf{0} \\ \mathbf{0} \\ \mathbf{0} \end{Bmatrix}$$

$$\mathbf{R}(\mathbf{V}; \mathbf{f}_t^*) = \begin{Bmatrix} \mathbf{Q}_B \\ \mathbf{Q}_t - \mathbf{q}_t + \mathbf{q}_t^* \end{Bmatrix} = \begin{Bmatrix} \mathbf{0} \\ \mathbf{0} \end{Bmatrix} \quad \text{for } \mathbf{V}_u = \mathbf{V}_u^*$$

$$\left(\frac{\partial \mathbf{R}}{\partial \mathbf{V}} \right)^{(n)} \Delta \mathbf{V}^{(n+1)} = -\mathbf{R}(\mathbf{V}^n; \mathbf{q}_t^*) - \Delta \mathbf{q}_t^*$$

$$\mathbf{R}(\mathbf{V}^0; \mathbf{f}_t^*) = \mathbf{0} \quad \mathbf{V}^{(n+1)} = \mathbf{V}^{(n)} + \Delta \mathbf{V}^{(n+1)}$$

Intel direct solver
PARDISO