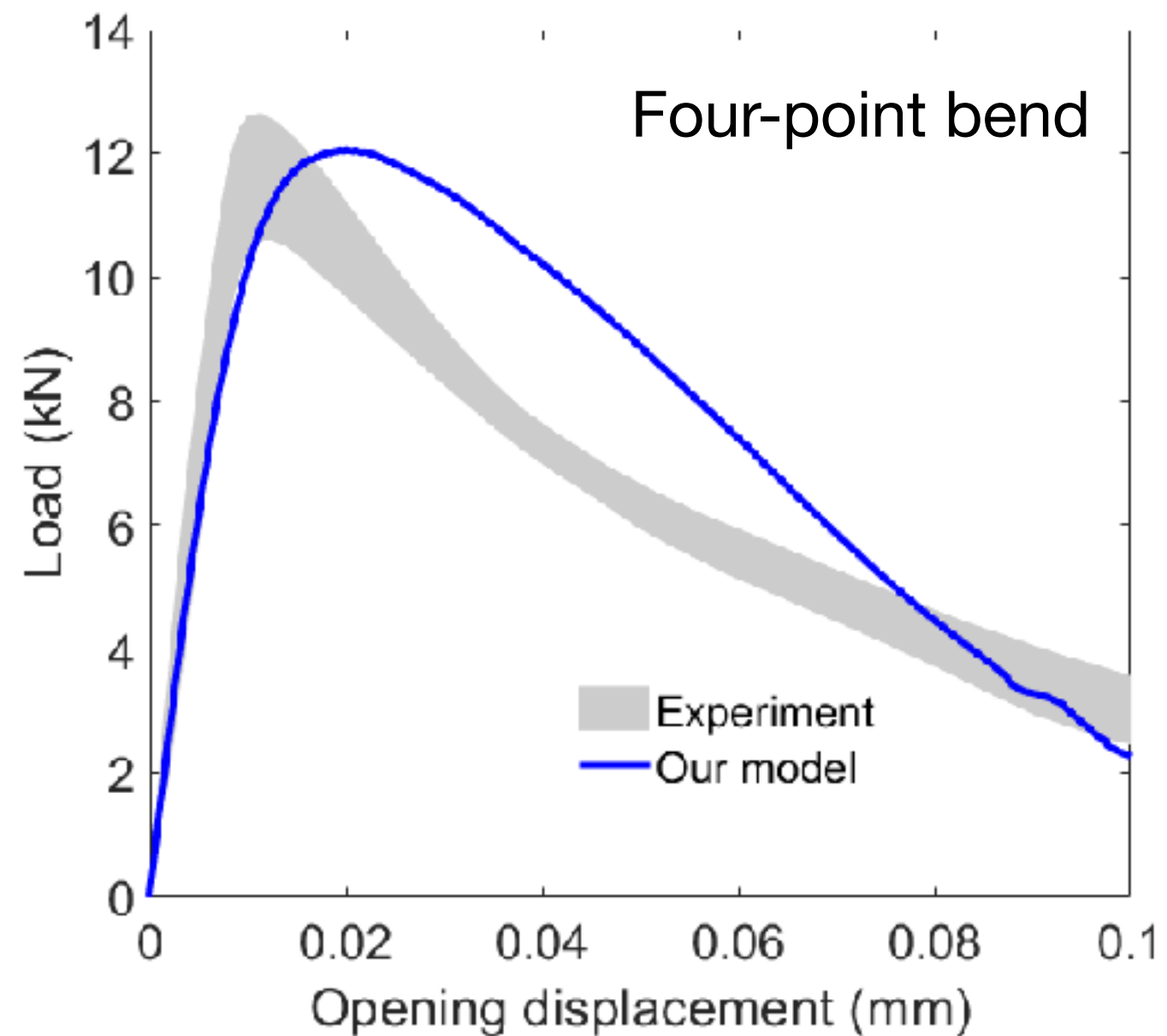
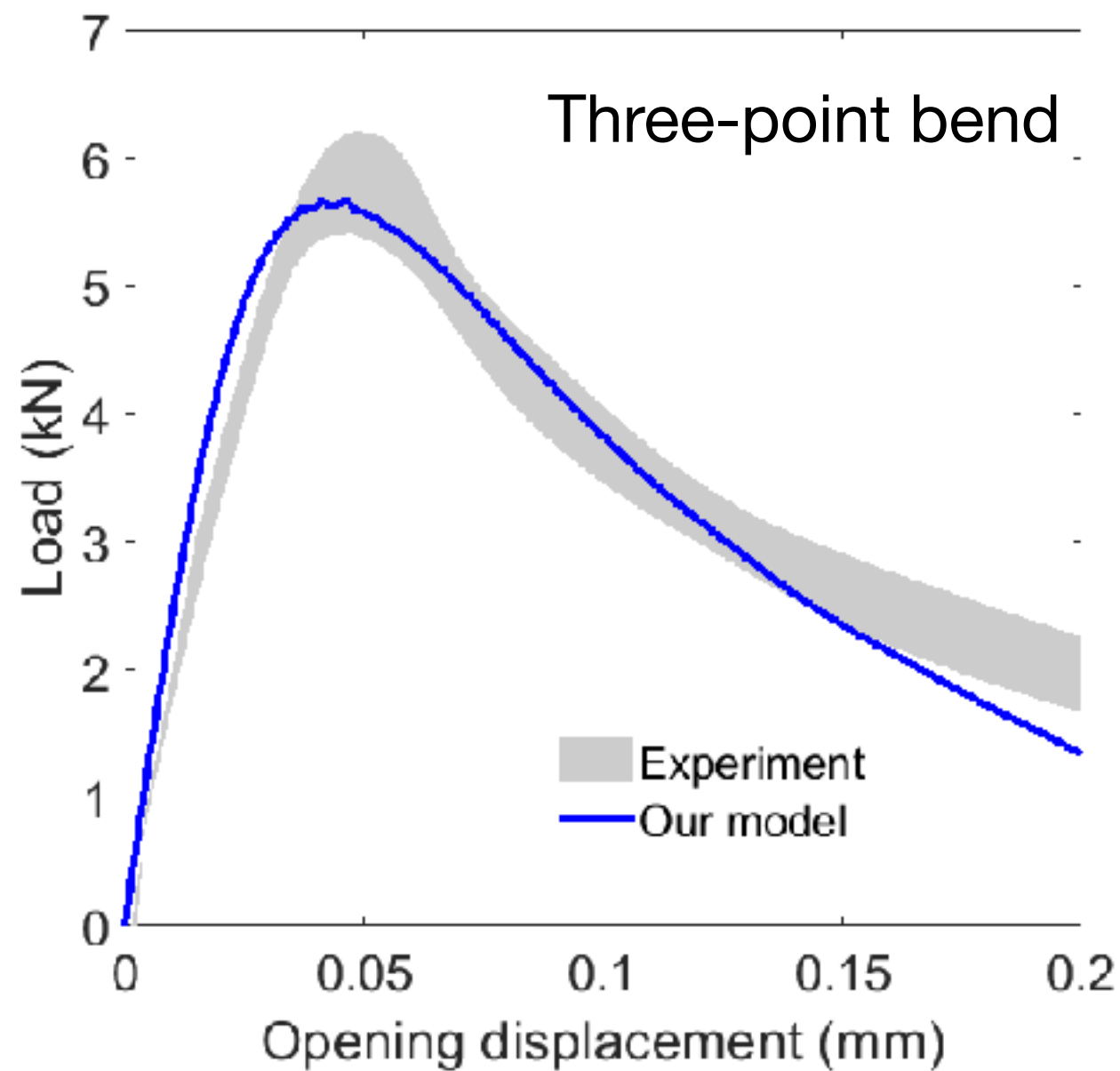


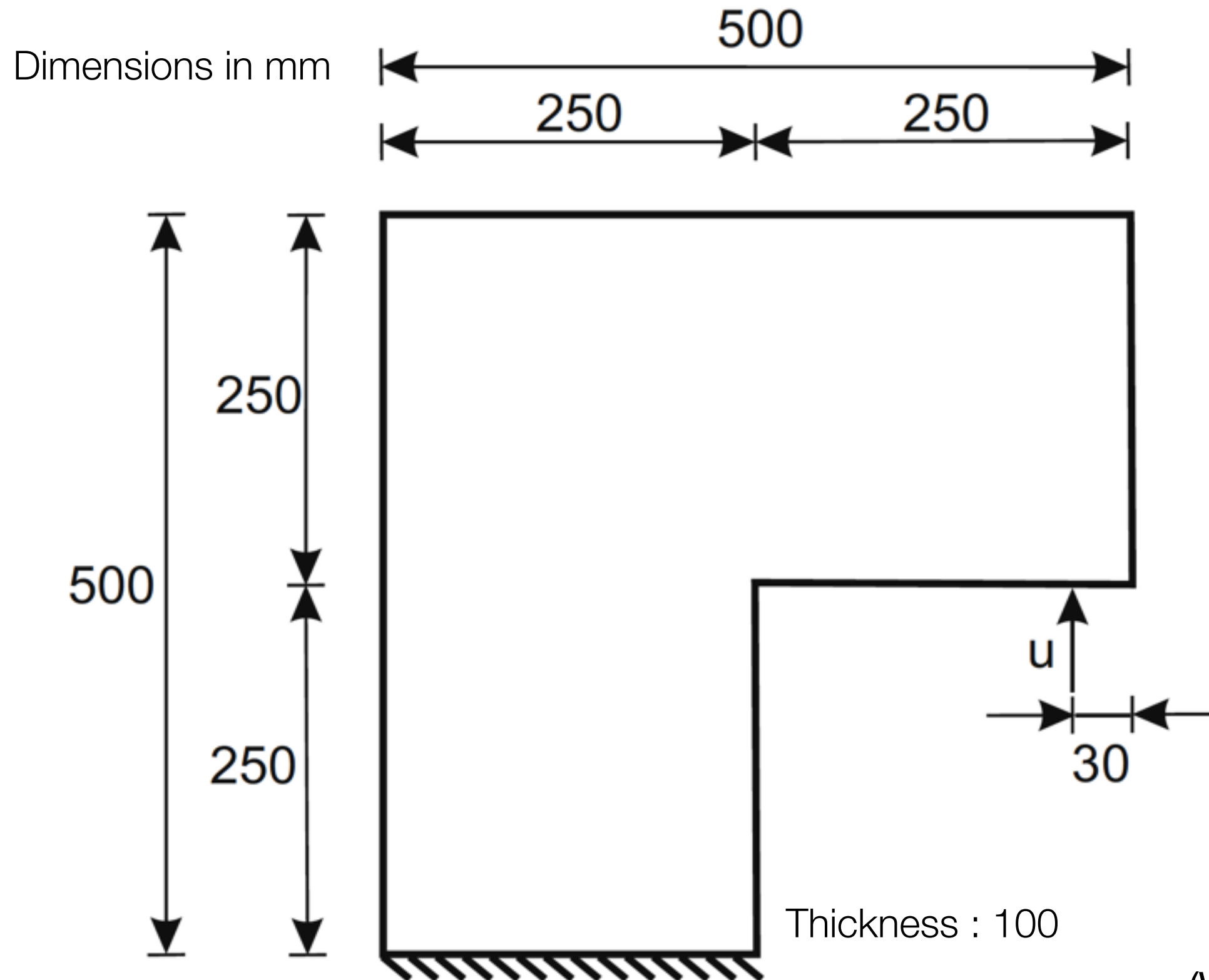
Asymmetric bend tests : Load-displacement comparison



Material Parameters

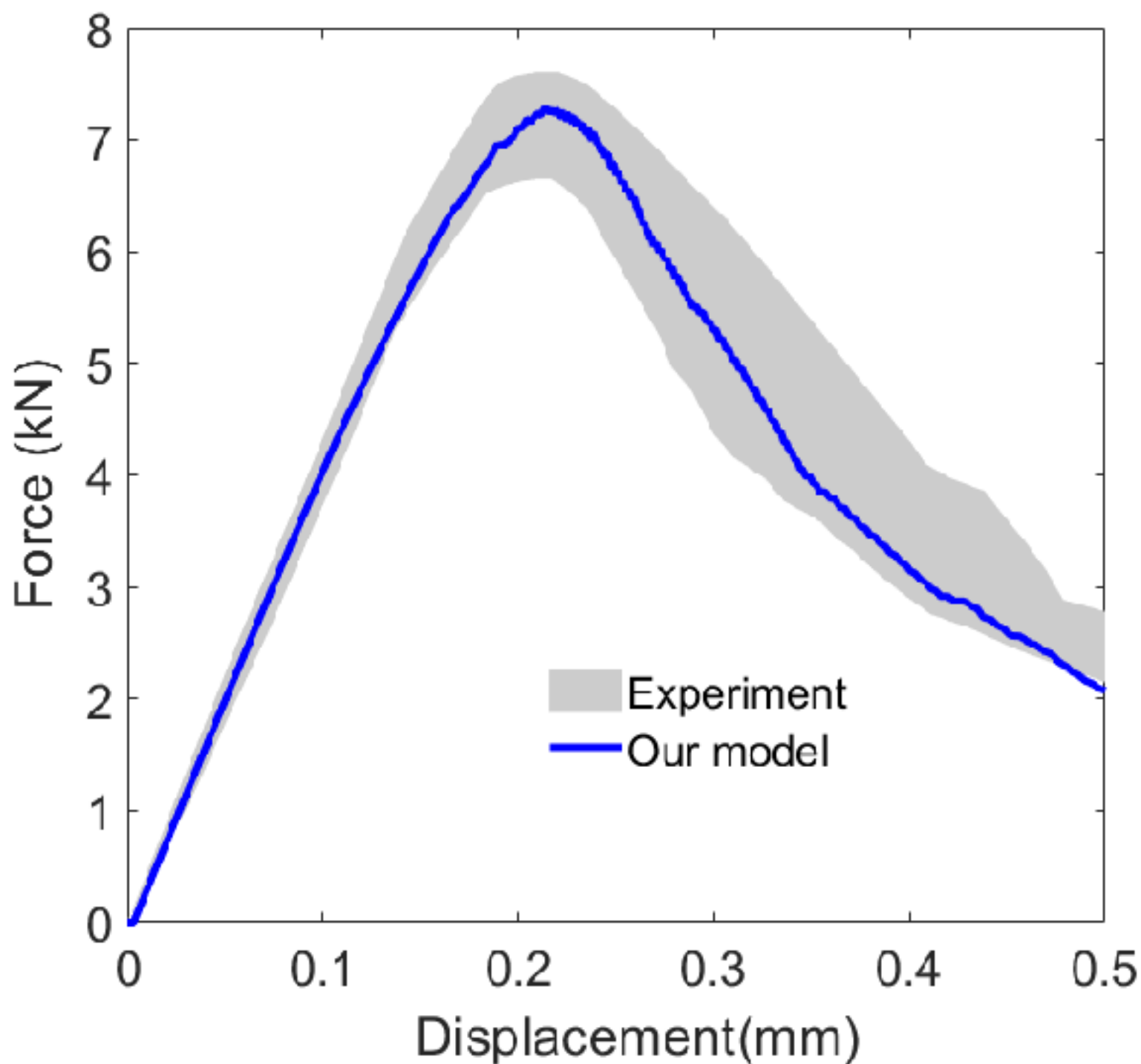
E	ν	S^c	κ	ϵ_{crit}^c	ψ_*	ℓ	ζ
38	0.2	3.1	0.7	2.5×10^{-4}	2.1	3	40
GPa	-	MPa	-	-	kJ/m^3	mm	kPa-s

L-shaped panel test



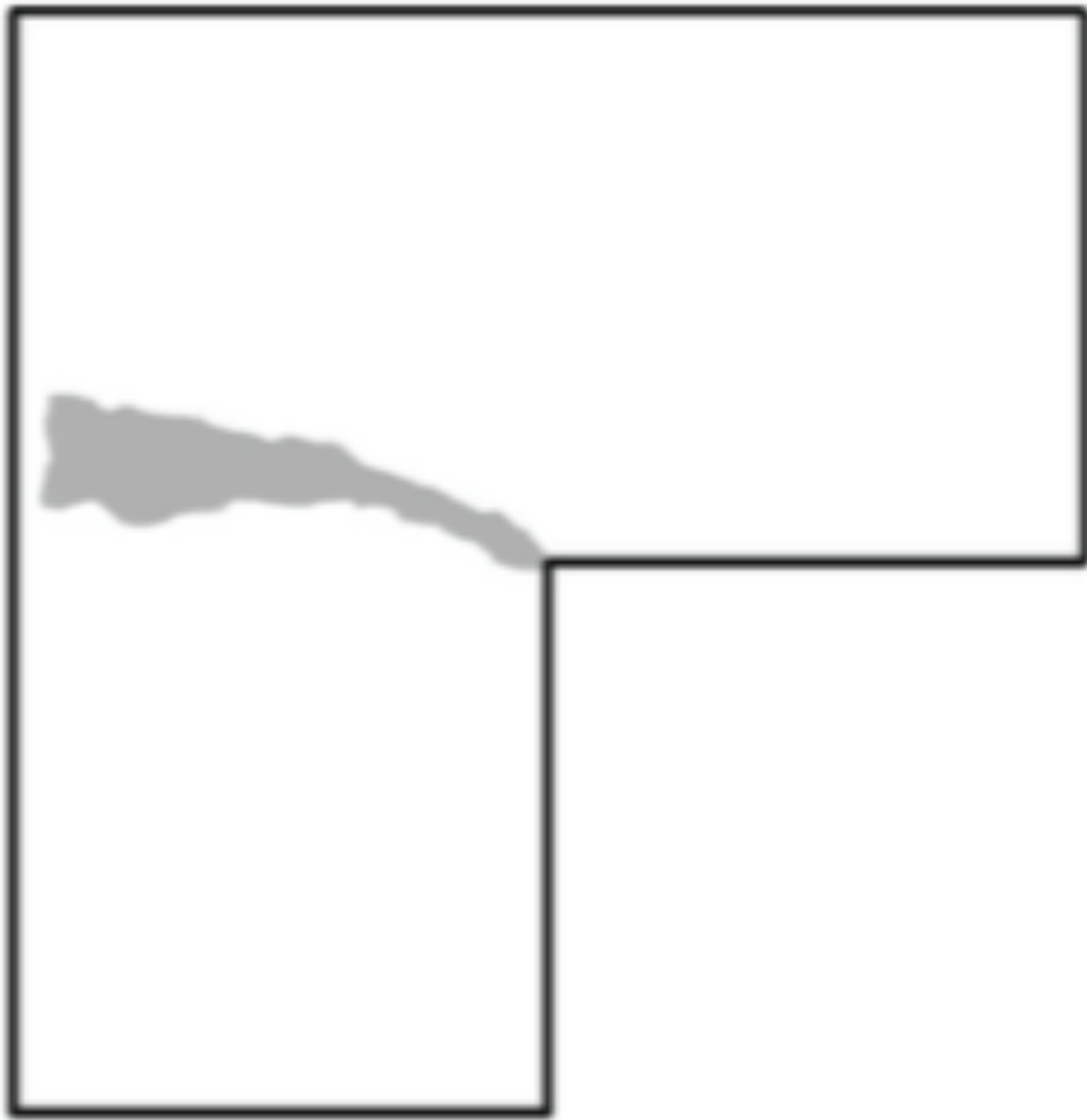
(Winkler, 2001)

L-shaped panel test

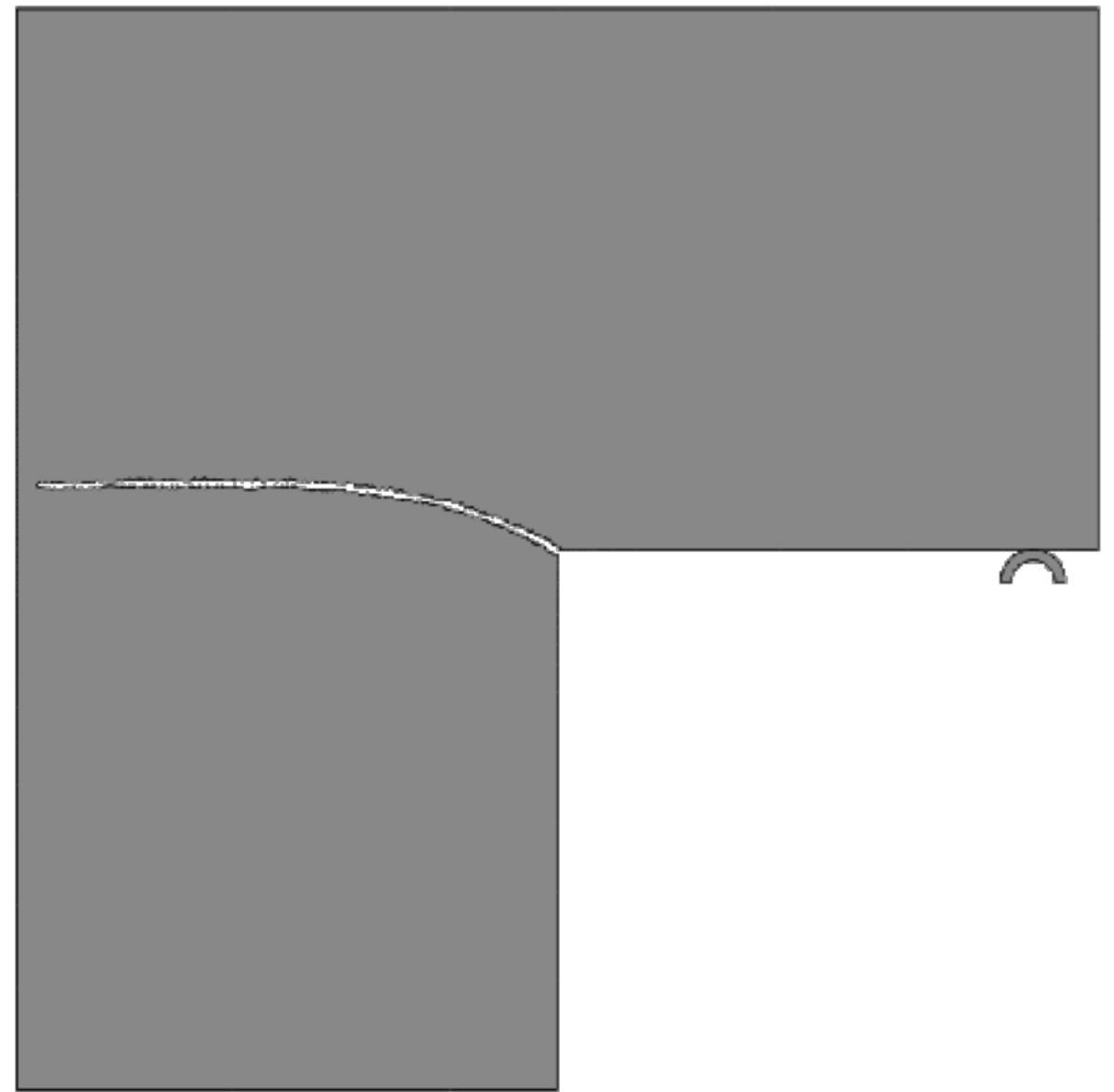


Material Parameters		
E	18	GPa
ν	0.18	-
S^c	2.5	MPa
\varkappa	0.7	-
ϵ_{crit}^c	4.9×10^{-4}	-
ψ_*	3.2	kJ/m^3
ℓ	4	mm
ζ	40	kPa-s

L-shaped panel test

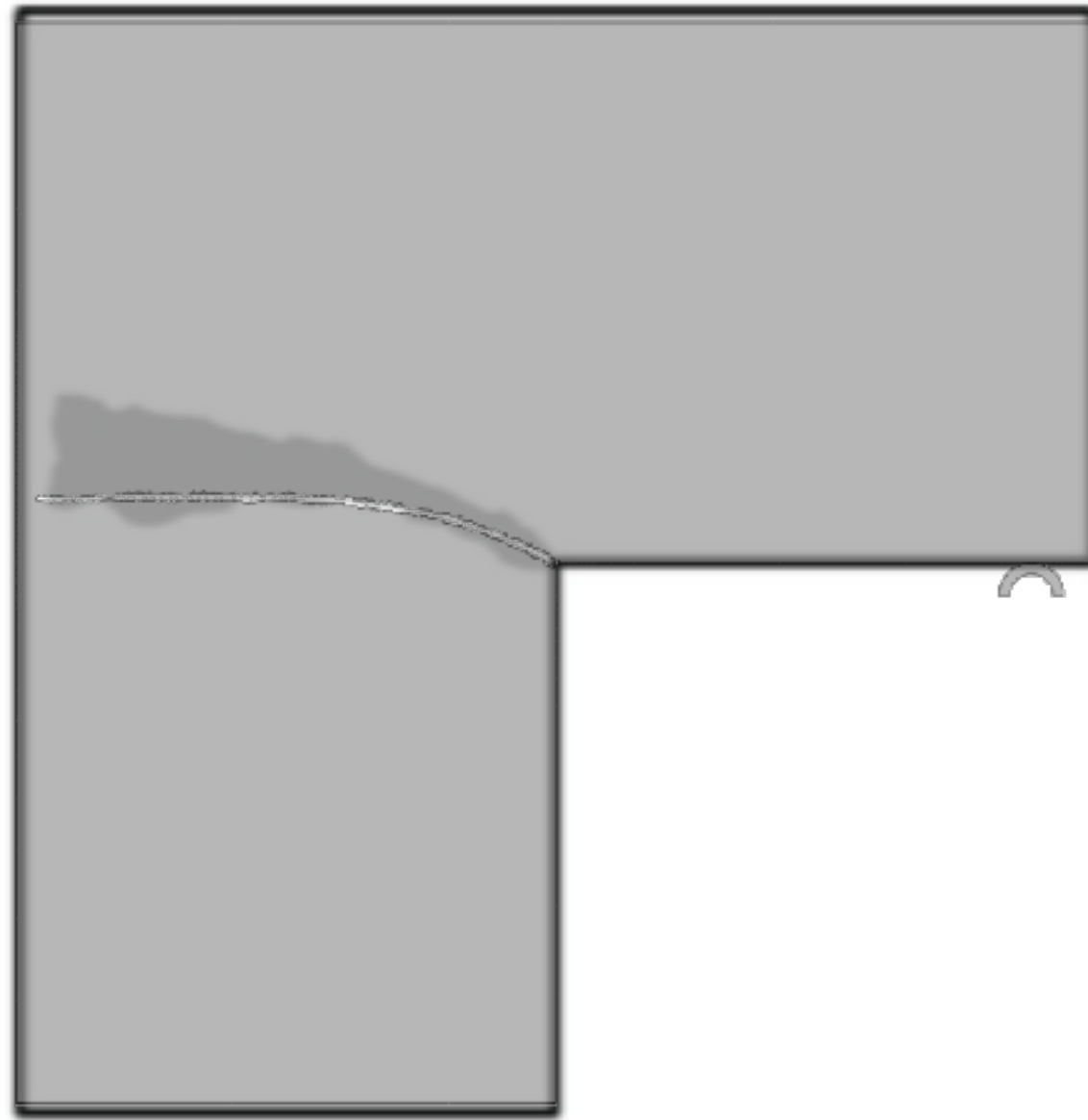


Experimentally observed crack pattern



Phase-field crack (our model)

L-shaped panel test



Phase field crack path overlaid against the
experimentally observed crack pattern

Concluding remarks

- We have formulated a new gradient-damage theory for modeling quasi-brittle fracture of concrete.
- Our theory goes beyond the existing phase-field theories for brittle fracture in that the theory:
 - allows for some amount of craze-type inelasticity prior to damage initiation, and that
 - it overcomes the need to decompose the energy into positive and negative contributions.
- The theory has been implemented numerically in ABAQUS as a user element subroutine (UEL).
- The theory has reasonably good predictive capabilities.
- Much more needs to be done.

A gradient-damage theory for fracture of elastomeric materials

Lallit Anand
with
Yunwei Mao and Brandon Talamini

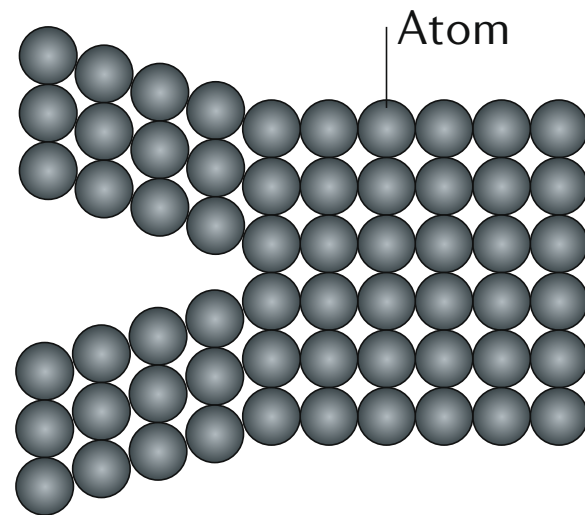
WFM 2020



**Massachusetts
Institute of
Technology**

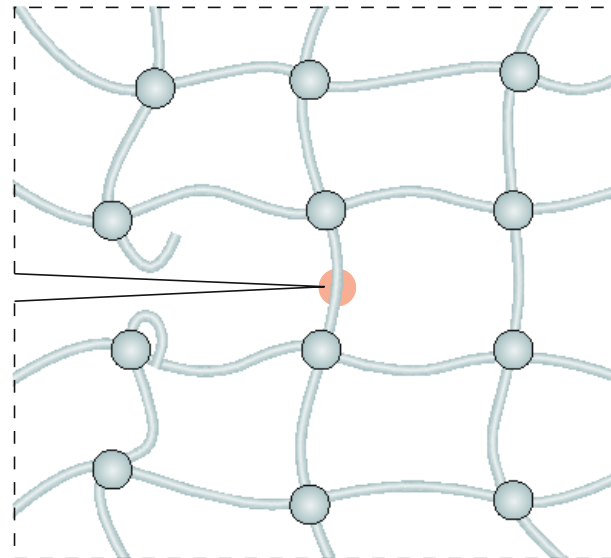
Fracture of elastomers

Griffith, 1921

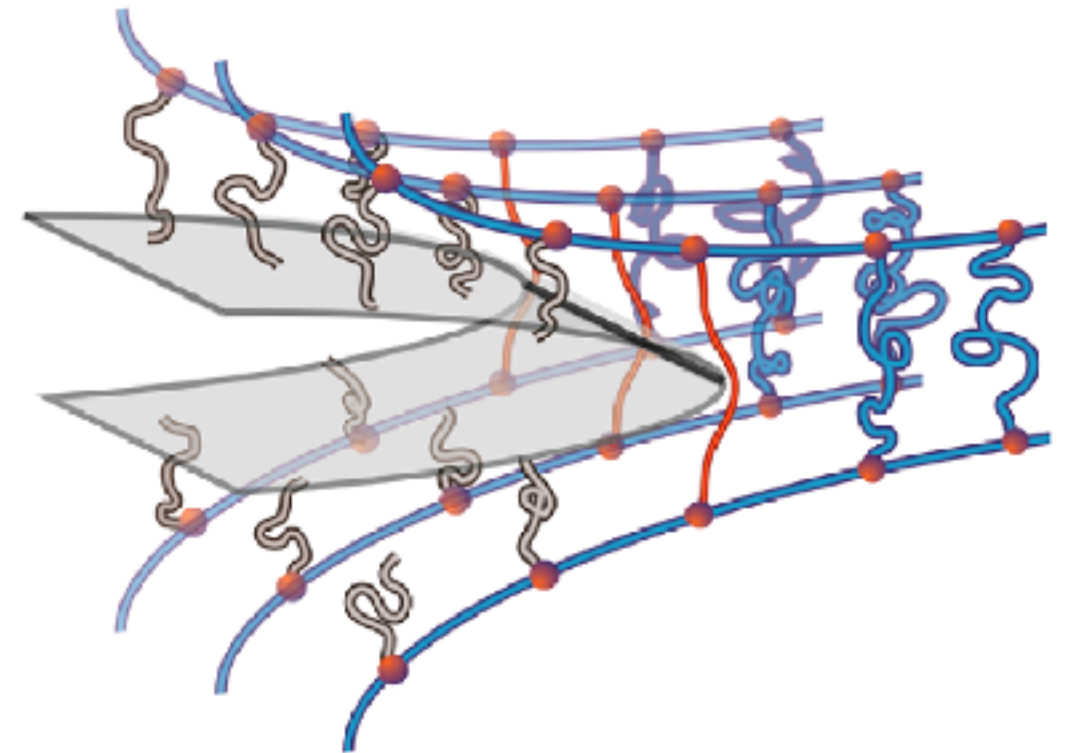


Crystalline materials
Break a layer of atoms
Toughness $\sim 1 \text{ J/m}^2$

Lake-Thomas 1967



Elastomeric materials
Snap a layer of chains
Toughness $\sim 10\text{-}1000 \text{ J/m}^2$



(From Yang & Suo, 2018)

- **Ideal** fracture by chain-scission of elastomeric materials with strong covalent crosslinks — in the spirit of Lake and Thomas (1967)
- Neglect any viscoelasticity or Mullin-type effects.

Modeling deformation of elastomeric materials

- For an isotropic material at a temperature ϑ the free-energy function is a symmetric function of the principal stretches λ_i ($i = 1, 2, 3$):

$$\psi_R = \hat{\psi}(\lambda_1, \lambda_2, \lambda_3, \vartheta), \quad J = \lambda_1 \lambda_2 \lambda_3 = 1.$$

- Effective stretch,

$$\bar{\lambda} \stackrel{\text{def}}{=} \frac{1}{\sqrt{3}} \sqrt{\lambda_1^2 + \lambda_2^2 + \lambda_3^2},$$

and consider a special free-energy,

$$\hat{\psi}_R(\bar{\lambda}; \vartheta).$$

- Since $\psi_R = \varepsilon_R - \vartheta \eta_R$,

$$\psi_R(\bar{\lambda}, \vartheta) = \varepsilon_R(\bar{\lambda}, \vartheta) - \vartheta \eta_R(\bar{\lambda}, \vartheta).$$

- For elastomeric materials the **internal energy is classically assumed to be independent of stretch** and a function of the temperature only,

$$\varepsilon_R = \hat{\varepsilon}_R(\vartheta),$$

and that the entropy is a separable function of temperature and the effective stretch

$$\eta_R = f(\vartheta) + g(\bar{\lambda}).$$

Arruda-Boyce free energy function

- A widely used free energy function is

$$\psi_R = -\theta\eta_R = G_0 \lambda_L^2 \left[\left(\frac{\bar{\lambda}}{\lambda_L} \right) \beta + \ln \left(\frac{\beta}{\sinh \beta} \right) \right], \quad \beta \stackrel{\text{def}}{=} \mathcal{L}^{-1} \left(\frac{\bar{\lambda}}{\lambda_L} \right),$$

where \mathcal{L}^{-1} is the function inverse of the Langevin function $\mathcal{L}(z) \stackrel{\text{def}}{=} \coth z - z^{-1}$.

- Two material parameters:

- Rubbery modulus,

$$G_0 = Nk_B\vartheta,$$

N — number of chains per unit reference volume.

- Network locking stretch,

$$\lambda_L = \sqrt{n}$$

n — number of links (Kuhn-segments) in each polymer chain.

- Generalized shear modulus: $G = G_0 \left(\frac{\lambda_L}{3\bar{\lambda}} \right) \mathcal{L}^{-1} \left(\frac{\bar{\lambda}}{\lambda_L} \right).$

- Since $\mathcal{L}^{-1}(z) \rightarrow \infty$ as $z \rightarrow 1$, the modulus $G \rightarrow \infty$ as $\bar{\lambda} \rightarrow \lambda_L$.

This response is pathological.