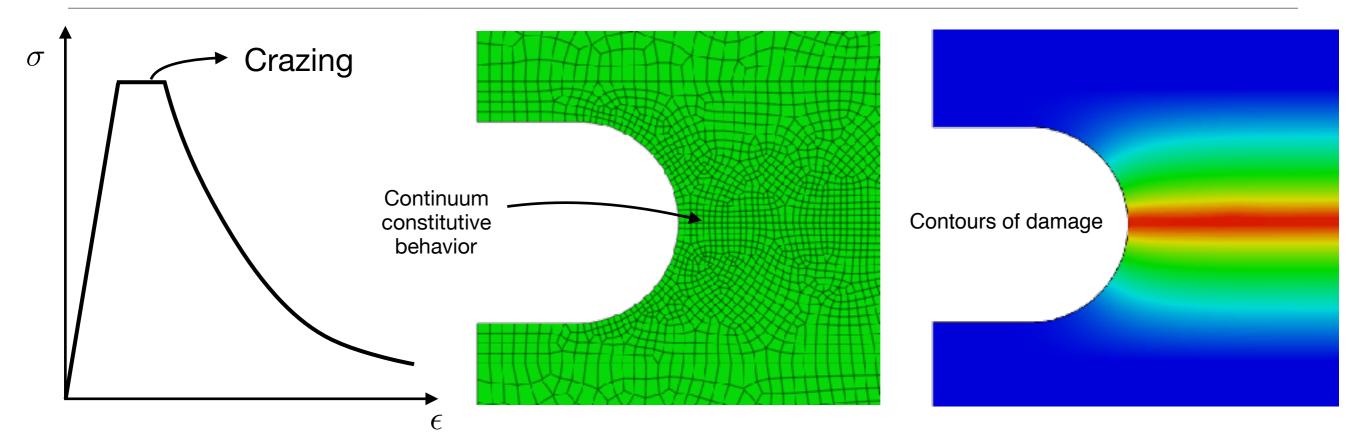
"Crazing" plus gradient-damage theory for quasi-brittle materials



- We introduce some "craze"-type inelasticity in the constitutive response of the material, prior to the damage/softening process.
- We use a gradient-damage theory.
 - A major reason for using a gradient-damage theory is to "regularize" the strain-softening behavior during the damaging process, and to avoid mesh-dependency related issues during finite element simulations.

Cf. the pioneering studies on fracture of quasi-brittle materials (e.g., Bazant, 1987; de Borst 1993; Peerlings et al., 1998), and also in the more recent phase-field theories of fracture of brittle materials (de Borst et al., 2016).

Gradient-damage theory

Kinematics

• Motion, deformation gradient, velocity, velocity gradient:

$$\chi(\mathbf{X},t), \quad \mathbf{F} = \nabla \chi, \quad \mathbf{v} = \dot{\chi}, \quad \mathbf{L} = \text{grad}\mathbf{v} = \dot{\mathbf{F}}\mathbf{F}^{-1}.$$

• Multiplicative decomposition of the deformation gradient:

$$\mathbf{F} = \mathbf{F}^e \mathbf{F}^c$$
,

- (i) $\mathbf{F}^c(\mathbf{X})$ with $J^c = \det \mathbf{F}^c > 0$ is the inelastic dilational distortion due to crazing, and
- (ii) $\mathbf{F}^e(\mathbf{X})$, with $J^e = \det \mathbf{F}^e > 0$ the elastic distortion.
- Craze flow:

$$\dot{\mathbf{F}}^c = \mathbf{D}^c \mathbf{F}^c$$
, $\mathbf{D}^c = \dot{\epsilon}^c \mathbf{N}^c$, with $\dot{\epsilon}^c = |\mathbf{D}^c| \ge 0$, $\mathbf{N}^c = \mathbf{m} \otimes \mathbf{m}$,

Velocity gradient:

$$\mathbf{L} = \mathbf{L}^e + \mathbf{F}^e \mathbf{D}^c \mathbf{F}^{e-1}, \qquad \Longrightarrow \qquad (\nabla \dot{\boldsymbol{\chi}}) \mathbf{F}^{-1} = \dot{\mathbf{F}}^e \mathbf{F}^{e-1} + \dot{\epsilon}^c \, \mathbf{F}^e \, \mathbf{N}^c \, \mathbf{F}^{e-1}.$$

• Damage variable,

$$d(\mathbf{X}, t) \in [0, 1],$$
 with $d(\mathbf{X}, t) \ge 0.$

Virtual power formulation of macroscopic and microscopic force balances

Rate-like kinematical descriptors. Internal and External power

$$(\nabla \dot{\boldsymbol{\chi}})\mathbf{F}^{-1} = \dot{\mathbf{F}}^e \mathbf{F}^{e-1} + \dot{\epsilon}^c \mathbf{F}^e \mathbf{N}^c \mathbf{F}^{e-1}, \quad \text{and} \quad \dot{\mathbf{d}} \ge 0.$$
 (†)

- The basic "rate-like" descriptors are the velocity $\dot{\chi}$, the elastic distortion rate $\dot{\mathbf{F}}^e$, the craze strain rate $\dot{\epsilon}^c$, and the damage rate $\dot{\mathbf{d}}$, and these are constrained by (\dagger) .
- Internal and external power:

$$\mathcal{W}_{\text{int}}(\mathsf{P}) = \int\limits_{\mathsf{P}} \left(\mathbf{S}^e : \dot{\mathbf{F}}^e + \pi \dot{\epsilon}^c + \varpi \dot{\mathsf{d}} + \boldsymbol{\xi} \cdot \nabla \dot{\mathsf{d}} \right) dv_{\mathsf{R}},$$

$$\mathcal{W}_{\text{ext}}(\mathsf{P}) = \int\limits_{\partial \mathsf{P}} \mathbf{t}_{\mathsf{R}}(\mathbf{n}_{\mathsf{R}}) \cdot \dot{\boldsymbol{\chi}} \, da_{\mathsf{R}} + \int\limits_{\mathsf{P}} \mathbf{b}_{\mathsf{R}} \cdot \dot{\boldsymbol{\chi}} \, dv_{\mathsf{R}} + \int\limits_{\partial \mathsf{P}} \xi(\mathbf{n}_{\mathsf{R}}) \, \dot{\mathbf{d}} \, da_{\mathsf{R}}.$$

